

AVIATION AND AERONAUTICAL ENGINEERING



Photo by Paul Thompson

General Joffre inspecting a Captured German Aeroplane

SEPTEMBER

15th
1916

SPECIAL FEATURES

MILITARY AEROPLANES
THE TRAINING OF MILITARY PILOTS
THEORY OF AN AEROPLANE ENCOUNTERING GUSTS
THE DUSENBERG AERO ENGINE
A GERMAN HYDROAEROPLANE
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SEPTEMBER 15, 1936

AVIATION

AND
AERONAUTICAL ENGINEERING

VOL. I. NO. 4

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HERBERT M. WILLIAMS, Jr.

Vol. 7

September 15, 1935

No. 8

THE leading article on the first page of this issue, "Military Aeroplanes," is so timely, the most important announcement that the War Department has ever issued in regard to aeroplanes in the United States Army. The chief of change of the Aviation Section of the Signal Corps, T. B. A., says of it in a letter addressed to AVIATION AND AERONAUTICAL ENGINEERING: "It is intended to create discussion," and dearest itself has that to say.

The purpose of this memorandum is to initiate a discussion . . .

We have no doubt that it will cause discussion in every quarter where men are to be found who take an interest in army aeroplanes. Many constructions will be started by the first announcement of the memorandum.

It is inherent that the type of aeroplane which all constructors have attempted to build at this country, the so-called 2 place reconnaissance tractor airplane with one motor, is a false development.

While this statement is heard to shock many American construction, there can be no question that the army officers who are responsible for it have based their conclusions upon an intimate knowledge of European success and failures.

The great standard which this memorandum will give is the building of fast single place machines and large two-motored tractor is evident from a cursory perusal. The specifications call for a speed of 115 miles an hour from a rotary mounted one place tractor, together with a climb of 10,000 feet in ten minutes, are severe in the extreme, yet the value of such a type of machine in operations against an enemy equipped with a real aerial war cannot be overestimated.

Armies are fairly conversant with the work of the French Army. The work of such men as Lieut. Wilbur Thies, Bert Ball, Elmer Cordia and Norman Prince, has shown that Americans are at least the equal of any other nation in the handling of speedy scout machines. The Army specifications for a "present" machine of great speed and with unusual climbing ability, will, if adhered to, make in any reasonable period of time give to the American Army a machine which the reconnaissance and independent of the American character can utilize to the best advantage.

The large slow two-motored machine which, according to the memorandum, will comprise 25 per cent of all the machines which we shall have to have in use of war, and which can be used as a scout machine, a bomber

for extreme long-range reconnaissance and for light work, entails many difficulties of construction. The gross effect of two-engines, in putting additional strain on the construction members of the landing chassis when bracing a machine of this type to earth, is but a single one of the subjects which will demand careful study.

The pleasure which AVIATION AND AERONAUTICAL ENGINEERING takes in submitting this memorandum to its readers cannot be exaggerated. Backed by an appropriation of \$13,281,600, Lieut. Colonel George G. Sapiro and his associates have set about building up an air-service for the army, with boundless experience and dispatch. All the lessons which our military air thought learned from the European war have been carefully digested, so that almost upon the heels of the signing of the appropriation bill we find the Aviation Section of the Signal Corps ready to give detailed information about its intentions and capabilities.

The general adoption of 25 per cent for all aeroplanes in our Army, Navy and National Guard, announced in our last issue, gave the first indication of the very real desire which the War Department is exhibiting to assist American constructors through standardization. The memorandum which is published in this issue goes much farther. Its effect in standardizing American military aeroplanes will be an unalloyed benefit to the industry. And yet the fact that in giving this article the publication the War Department announces that "the purpose is to initiate discussion," proves that those in control still have open minds for future developments.

In view of this desire on the part of the War Department to obtain expressions of opinion, AVIATION AND AERONAUTICAL ENGINEERING will be glad to open its columns to all constructors of aeroplanes and aeroplane engines who care to use them to discuss the War Department's memorandum. Diagrams of aeroplanes and aeromarine motors are urged to send AVIATION AND AERONAUTICAL ENGINEERING their opinions and criticisms. Open discussion of all technical articles appearing in our issue will always be welcomed. The more points of view that can be secured, the more valuable will each issue be to the aeronautical industry.

Every manufacturer of aeroplanes and aeroplane engines should be grateful to the War Department for its prospectus in making this announcement. Everyone interested in the industry will await eagerly the publication of the detailed specifications for the six types of aeroplanes and four types of aeroplane motors, which the memorandum states, the Army will need.

The Training of Military Pilots

By Lieutenant Phillips Roder

Military aviation is still in its infancy. At present no one can predict the possibilities of its future. It is a vast subject, covering practically every branch of military service, and requiring every form of technical knowledge and engineering skill.

[illegible]

Actual flying is only a very small part of the training a good service pilot needs to do. He should have at least six months' general and technical training before he is even allowed to fly.

[illegible]

The new idea after the paper has proved to be communicating their own ability as the above explained is to put her through a course of work. He should learn the Morse code thoroughly, and also the plain text codes of the army. He should pass written examinations in the construction and theory of wireless telegraphy and telephony. He should be capable of working an entire set himself. He is then ready for the next

The paper should now be sent on a two weeks' course as a machine gun school, where he is instructed in the elements, taking down and putting together of the latest types of machine guns. He should know which part is liable to jam in the air, as ignorance in that subject could easily cost him his life in an actual combat.

The next move is to gain a practical working knowledge of aerial photography, just when and where to take good pictures of military value.

Now comes the struggle to change. The paper could learn how to take down, tune, and repair every type of engine and be his government. He should have the practical knowledge his classmates have. The coding system, magazine, business and printing should all be very carefully studied as to forced learning this is a great asset, and will often save the government thousands of dollars. Goodbye reconstruction is another place to be studied.

Smiling is almost as essential as shaking. A good server-poke should know the stranger (shook, left). Balance and grace

of the characteristics of all materials in use in his area. He should be able to tell at a glance whether a material was designed for a particular purpose. The inside strength of a material should be known, and a general knowledge of the properties of materials is advisable. Fabrics and clays should be studied and various woods studied for lightness and toughness. A work area in a woodworking shop would suffice. A collection of bricks and stone, stones, slugs, shells and metals should be examined and studied for strength and elasticity. Various types of glues and setting applications, such as in sculpture, should be studied. The subject can be taken in many ways. If all of this is considered the pupil may be taken to appreciate the two first lights.

Slightly over a quarter of a century has its own special method. Some are excellent, and some are poor. While commenting on the merits or demerits of my own system I have been through the experience of trying hundreds of methods, and the majority have turned out excellent results.

In the first 10 types I believe in accumulating the things you get, getting the paper used by the boy and his mother, and showing what can be done at the age with an average intelligence. This usually involves a few central books, nothing more than the average boy would read. The average intelligence is five. The paper is now made for his first and last readings. This usually consists of 10 readings. That is, in 10 or 15 or 20 or 30 or 40 or 50 or 60 or 70 or 80 or 90 or 100 or 110 or 120 or 130 or 140 or 150 or 160 or 170 or 180 or 190 or 200 or 210 or 220 or 230 or 240 or 250 or 260 or 270 or 280 or 290 or 300 or 310 or 320 or 330 or 340 or 350 or 360 or 370 or 380 or 390 or 400 or 410 or 420 or 430 or 440 or 450 or 460 or 470 or 480 or 490 or 500 or 510 or 520 or 530 or 540 or 550 or 560 or 570 or 580 or 590 or 600 or 610 or 620 or 630 or 640 or 650 or 660 or 670 or 680 or 690 or 700 or 710 or 720 or 730 or 740 or 750 or 760 or 770 or 780 or 790 or 800 or 810 or 820 or 830 or 840 or 850 or 860 or 870 or 880 or 890 or 900 or 910 or 920 or 930 or 940 or 950 or 960 or 970 or 980 or 990 or 1000 or 1010 or 1020 or 1030 or 1040 or 1050 or 1060 or 1070 or 1080 or 1090 or 1100 or 1110 or 1120 or 1130 or 1140 or 1150 or 1160 or 1170 or 1180 or 1190 or 1200 or 1210 or 1220 or 1230 or 1240 or 1250 or 1260 or 1270 or 1280 or 1290 or 1300 or 1310 or 1320 or 1330 or 1340 or 1350 or 1360 or 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2620 or 2630 or 2640 or 2650 or 2660 or 2670 or 2680 or 2690 or 2700 or 2710 or 2720 or 2730 or 2740 or 2750 or 2760 or 2770 or 2780 or 2790 or 2800 or 2810 or 2820 or 2830 or 2840 or 2850 or 2860 or 2870 or 2880 or 2890 or 2900 or 2910 or 2920 or 2930 or 2940 or 2950 or 2960 or 2970 or 2980 or 2990 or 3000 or 3010 or 3020 or 3030 or 3040 or 3050 or 3060 or 3070 or 3080 or 3090 or 3100 or 3110 or 3120 or 3130 or 3140 or 3150 or 3160 or 3170 or 3180 or 3190 or 3200 or 3210 or 3220 or 3230 or 3240 or 3250 or 3260 or 3270 or 3280 or 3290 or 3300 or 3310 or 3320 or 3330 or 3340 or 3350 or 3360 or 3370 or 3380 or 3390 or 3400 or 3410 or 3420 or 3430 or 3440 or 3450 or 3460 or 3470 or 3480 or 3490 or 3500 or 3510 or 3520 or 3530 or 3540 or 3550 or 3560 or 3570 or 3580 or 3590 or 3600 or 3610 or 3620 or 3630 or 3640 or 3650 or 3660 or 3670 or 3680 or 3690 or 3700 or 3710 or 3720 or 3730 or 3740 or 3750 or 3760 or 3770 or 3780 or 3790 or 3800 or 3810 or 3820 or 3830 or 3840 or 3850 or 3860 or 3870 or 3880 or 3890 or 3900 or 3910 or 3920 or 3930 or 3940 or 3950 or 3960 or 3970 or 3980 or 3990 or 4000 or 4010 or 4020 or 4030 or 4040 or 4050 or 4060 or 4070 or 4080 or 4090 or 4100 or 4110 or 4120 or 4130 or 4140 or 4150 or 4160 or 4170 or 4180 or 4190 or 4200 or 4210 or 4220 or 4230 or 4240 or 4250 or 4260 or 4270 or 4280 or 4290 or 4300 or 4310 or 4320 or 4330 or 4340 or 4350 or 4360 or 4370 or 4380 or 4390 or 4400 or 4410 or 4420 or 4430 or 4440 or 4450 or 4460 or 4470 or 4480 or 4490 or 4500 or 4510 or 4520 or 4530 or 4540 or 4550 or 4560 or 4570 or 4580 or 4590 or 4600 or 4610 or 4620 or 4630 or 4640 or 4650 or 4660 or 4670 or 4680 or 4690 or 4700 or 4710 or 4720 or 4730 or 4740 or 4750 or 4760 or 4770 or 4780 or 4790 or 4800 or 4810 or 4820 or 4830 or 4840 or 4850 or 4860 or 4870 or 4880 or 4890 or 4900 or 4910 or 4920 or 4930 or 4940 or 4950 or 4960 or 4970 or 4980 or 4990 or 5000 or 5010 or 5020 or 5030 or 5040 or 5050 or 5060 or 5070 or 5080 or 5090 or 5100 or 5110 or 5120 or 5130 or 5140 or 5150 or 5160 or 5170 or 5180 or 5190 or 5200 or 5210 or 5220 or 5230 or 5240 or 5250 or 5260 or 5270 or 5280 or 5290 or 5300 or 5310 or 5320 or 5330 or 5340 or 5350 or 5360 or 5370 or 5380 or 5390 or 5400 or 5410 or 5420 or 5430 or 5440 or 5450 or 5460 or 5470 or 5480 or 5490 or 5500 or 5510 or 5520 or 5530 or 5540 or 5550 or 5560 or 5570 or 5580 or 5590 or 5600 or 5610 or 5620 or 5630 or 5640 or 5650 or 5660 or 5670 or 5680 or 5690 or 5700 or 5710 or 5720 or 5730 or 5740 or 5750 or 5760 or 5770 or 5780 or 5790 or 5800 or 5810 or 5820 or 5830 or 5840 or 5850 or 5860 or 5870 or 5880 or 5890 or 5900 or 5910 or 5920 or 5930 or 5940 or 5950 or 5960 or 5970 or 5980 or 5990 or 6000 or 6010 or 6020 or 6030 or 6040 or 6050 or 6060 or 6070 or 6080 or 6090 or 6100 or 6110 or 6120 or 6130 or 6140 or 6150 or 6160 or 6170 or 6180 or 6190 or 6200 or 6210 or 6220 or 6230 or 6240 or 6250 or 6260 or 6270 or 6280 or 6290 or 6300 or 6310 or 6320 or 6330 or 6340 or 6350 or 6360 or 6370 or 6380 or 6390 or 6400 or 6410 or 6420 or 6430 or 6440 or 6450 or 6460 or 6470 or 6480 or 6490 or 6500 or 6510 or 6520 or 6530 or 6540 or 6550 or 6560 or 6570 or 6580 or 6590 or 6600 or 6610 or 6620 or 6630 or 6640 or 6650 or 6660 or 6670 or 6680 or 6690 or 6700 or 6710 or 6720 or 6730 or 6740 or 6750 or 6760 or 6770 or 6780 or 6790 or 6800 or 6810 or 6820 or 6830 or 6840 or 6850 or

[illegible][illegible]

Night flying is another very important and most difficult branch of military aviation. In England to-day no man who is being trained for night work as service pilots are being trained for the front.

After all of those various phases have been learned and accomplished, then, and not before, is a man qualified to be called an efficient service pilot. There is indeed a survival of the fittest, but nevertheless a good service pilot is made, not born.

Theory of an Aeroplane Encountering Gusts*

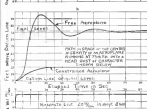
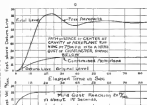
(E-mail: graham@maths.usyd.edu.au)

By Professor E. H. Wilson

Revised by Alexander Adams

It is not proposed to publish in any detail the author's methods which Professor Wilson employs in his brilliant analysis. For an understanding of these methods, long preliminary study of atmospheric stability treated in the more rigorous fashion of Plesner, Holtslag, and Hummel is necessary, and even then the complete survey of the paper would require far more time and effort than the busy aeronautical engineer can afford. It would be fortunate if the small interested community.

It was Professor Wilson's problem at the first place to indicate the action of growth is functional factors which could be



Comparative Effects of Hires as Contractors and Employees on Large-Scale Mergers

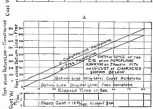
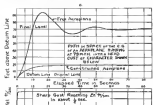
described into the differential equations in terms of the population, so that the former could stand in nearly isolation for the purpose the author approximated the growth of the mass in that of exponential functions with varying values in parallel cases of greater or lower rapidly of growth. It might be observed that growth did not follow any exponential function nor any regular function and the more serious of the latter function does, a small from a very unusual heterogeneity. If the exponential curve are compared with actual heterogeneity and growth, a decided nonconformity is there which is noticed.

It is true that no good ever rises to a maximum and stops there, and the study of the effects of gusts of expenditure fur-

¹ To be the subject of the 271025-2 to some extent, and I to the time by means.

gives a very fair idea of what would be the behavior of a spinnaker on striking a gust of similar character in flight, and a still better method of comparing the behavior of machines provided with a gyroscope stabilizer, and of machines without one.

The assumptions of the paper also differ from the facts of nature in so far as the air is taken to be still with uniform gusts, whereas generally speaking the air is never still, and gusts of varying intensity are superimposed on a steady wind that has probably little importance.



The actual motion was of the form $J(t) = J_0 \sin \omega t$, where J_0 was the maximum value of the force actually measured. To increase the value of ν , the amplitude value of J was increased and the summer in the maximum value obtained. This function ν is taken as superimposed on the natural oscillation of the machine. The equations of motion are solved by standard mathematical methods assuming considerable labor. Expressions for the resulting values in horizontal and vertical directions, and for rotary or pitching velocity, are derived and then integrated to form the path in space of the machine and also its acceleration.

1. A machine uncontrolled by the pilot, and unconstrained by any mechanical stability device.

Flat Plates. Simple Problems on Sustentation and Resistance of Wing Surfaces

Coefficients of Resistance for Circular or Square Plates Normal to the Wind, Varying Speeds

Although it would seem that the question of the forces on a flat plate placed normally to the wind would be fundamental in aerodynamics, and although it can be shown by the principle of dynamical similarity that similar plates should have the same coefficients no matter what their size, provided that all conditions remain, yet considerable controversy exists as to the variation in the values with the area of plate and with the velocity of flow. Those who are interested in the central and most important of the question are referred to the references at the end of the section. For all practical purposes, the following table may be safely used:

$R = K A V^2$ where R = resistance on pounds
 A = area of plate in square feet
 V = velocity in miles per hour.

TABLE 1

Ratio of Velocity of Flow to Velocity of Plate	K
0.5	0.00265
1.0	0.00265
1.5	0.00265
2.0	0.00265
3.0	0.00265
5.0	0.00265
10.0	0.00265

Coefficients for Rectangular Flat Plates Normal to the Wind, Varying Aspect Ratio

The aspect ratio of a flat plate is the ratio of b to a , as shown in the Fig. 1. With increased aspect ratio the resistance coefficient decreases. A theoretical estimate of the resistance coefficient of a flat plate is the ratio of the area of the plate to the area of the wind, which is the area of the plate. The following table shows the effect of increased aspect ratio, assuming the resistance coefficient to be the same for a square plate of the same area as taken in Table 1.

TABLE 2

Aspect Ratio	K for Rectangular Plate
1.0	0.00265
1.5	0.00265
2.0	0.00265
3.0	0.00265
5.0	0.00265
10.0	0.00265
20.0	0.00265
50.0	0.00265
100.0	0.00265

These values are plotted in Fig. 3 and are assumed to be true independently of the size of the plate.

* This course originated in the summer 1914, being an extension of the course in aerodynamics given by the author in the summer of 1913. It is intended to be a practical course in aerodynamics, and is intended to be a practical course in aerodynamics.

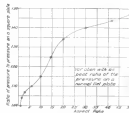


FIG. 3. VARIATION WITH ASPECT RATIO OF THE PRESSURE ON A WING FLAT PLATE

Coefficients of Resistance for Flat Plates Inclined to the Wind

Table 3 gives values for K , A , and L/R and Table 4 the distances of the center of the pressure from the leading edge of the plate in terms of the chord, for flat plates of various aspect ratios. The drag at 90° may be calculated from values of K for side resistance.

TABLE 3

Aspect Ratio	K	A	L/R	Aspect Ratio	K	A	L/R
1.0	0.00265	0.00265	0.1	10	0.00265	0.00265	1.0
1.5	0.00265	0.00265	0.15	15	0.00265	0.00265	1.5
2.0	0.00265	0.00265	0.2	20	0.00265	0.00265	2.0
3.0	0.00265	0.00265	0.3	30	0.00265	0.00265	3.0
5.0	0.00265	0.00265	0.5	50	0.00265	0.00265	5.0
10.0	0.00265	0.00265	1.0	100	0.00265	0.00265	10.0

Aspect Ratio	K	A	L/R	Aspect Ratio	K	A	L/R
1.0	0.00265	0.00265	0.1	10	0.00265	0.00265	1.0
1.5	0.00265	0.00265	0.15	15	0.00265	0.00265	1.5
2.0	0.00265	0.00265	0.2	20	0.00265	0.00265	2.0
3.0	0.00265	0.00265	0.3	30	0.00265	0.00265	3.0
5.0	0.00265	0.00265	0.5	50	0.00265	0.00265	5.0
10.0	0.00265	0.00265	1.0	100	0.00265	0.00265	10.0

Aspect Ratio	K	A	L/R	Aspect Ratio	K	A	L/R
1.0	0.00265	0.00265	0.1	10	0.00265	0.00265	1.0
1.5	0.00265	0.00265	0.15	15	0.00265	0.00265	1.5
2.0	0.00265	0.00265	0.2	20	0.00265	0.00265	2.0
3.0	0.00265	0.00265	0.3	30	0.00265	0.00265	3.0
5.0	0.00265	0.00265	0.5	50	0.00265	0.00265	5.0
10.0	0.00265	0.00265	1.0	100	0.00265	0.00265	10.0

Aspect Ratio	K	A	L/R	Aspect Ratio	K	A	L/R
1.0	0.00265	0.00265	0.1	10	0.00265	0.00265	1.0
1.5	0.00265	0.00265	0.15	15	0.00265	0.00265	1.5
2.0	0.00265	0.00265	0.2	20	0.00265	0.00265	2.0
3.0	0.00265	0.00265	0.3	30	0.00265	0.00265	3.0
5.0	0.00265	0.00265	0.5	50	0.00265	0.00265	5.0
10.0	0.00265	0.00265	1.0	100	0.00265	0.00265	10.0

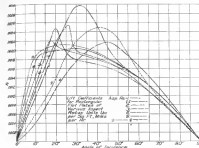


FIG. 4. LIFT COEFFICIENTS FOR RECTANGULAR FLAT PLATES IN VARIOUS ASPECT RATIOS

TABLE 4

Aspect Ratio	K	A	L/R	Aspect Ratio	K	A	L/R
1.0	0.00265	0.00265	0.1	10	0.00265	0.00265	1.0
1.5	0.00265	0.00265	0.15	15	0.00265	0.00265	1.5
2.0	0.00265	0.00265	0.2	20	0.00265	0.00265	2.0
3.0	0.00265	0.00265	0.3	30	0.00265	0.00265	3.0
5.0	0.00265	0.00265	0.5	50	0.00265	0.00265	5.0
10.0	0.00265	0.00265	1.0	100	0.00265	0.00265	10.0

In Fig. 4 are plotted values of K , aspect ratio of rectangles for various aspect ratios. In Fig. 4 the same treatment is applied to the L/R ratio.

In Fig. 5 are indicated the positions of the center of pressure for various aspect ratios and angles of incidence. In Fig. 6 the distances and points of application of the resultant forces are indicated for a flat plate of aspect ratio 10—the value which is usually employed for purposes of comparison—only to give the reader a more graphic idea of the forces at play.

In all these values it may be noted that as the angle of incidence increases the resistance coefficient increases with the area of plate, and this is probably accurate enough for all practical purposes.

Preliminary Application of Data for Flat Plates in Rudder and Elevator Design

These curves and tables give fairly complete data for the flat plate and are likely to meet all the requirements of design. It may be useful to indicate a few other points, and to make preliminary reference to the design of flat rudders and elevators.

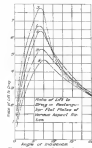


FIG. 5. RATIO OF LIFT TO DRAG IN RECTANGULAR FLAT PLATES IN VARIOUS ASPECT RATIOS

- (1) For plates of all aspect ratios when turned from zero angle, the lift increases until the critical angle or "burble point" is reached. Beyond this angle the lift rapidly decreases, and no rudder or elevator should be employed beyond this critical angle.
- (2) The lift drag ratio is not much improved, for flat plates of the same angles, by increased aspect ratio. For all plates

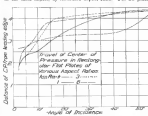


FIG. 6. TABLE OF CENTER OF PRESSURE IN RECTANGULAR FLAT PLATES OF VARIOUS ASPECT RATIOS

the ratio increases in maximum value at small angles, 5° to 7° . At angles still smaller it decreases, due to the predominating effect of the skin friction. Plates of large aspect ratio, being more sensitive at small angles, are, on the whole, more efficient in flight.

(3) On the other hand, plates of small aspect ratio have the critical angle much later and give a wider range of action. They also give a more highly lift at the critical angle, which is important in the action of the rudder when "burbling" at less speeds on the ground.

- (4) For the elevator, which is most conveniently used in the down position, the greatest lifting power is not required on the ground, as aspect ratio of three means a fair compromise.
- (5) For the rudder, the above considerations seem to indicate an aspect ratio of one or two is advisable.
- (6) It should be noted that, as the angle of incidence is increased, not only does the force increase, but also that from



FIG. 6. INCREASE SHEDDING, DRAG AND POWER IN AERIAL CURVES OF DIFFERENT FORMS IN A RECTANGULAR FLAT PLANE AT ANGLE RAYED AT NORMAL AND ONE OF INCIDENCE

the point of application of the resultant force in the hinge, giving a greatly increased moment about the hinge. If either the elevator or the rudder is placed too near the wings it accumulates large areas for the controlling surfaces, and the pilot may have to exert tremendous forces at large angles.

(7) To obtain the accuracy of steering large forces on the controls, it is possible to use a balanced rudder, one in which the hinge is placed about in the position of the center of pressure at small angles. The rudder on Fig. 7 is a balanced rudder. It should be noted that the "balancer" is only approximate.

Problems on Flat Plane

A rectangular flat plane 4 feet 6 inches high and 4 feet 3 inches long is employed as a rudder, and is placed with its leading edge at a distance of 16 feet from the center of gravity.

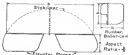


FIG. 7. DIAGRAM FOR ANGLE RAYED IN RUDDER AND ELEVATOR

of the surface. The surface is traveling at 60 miles an hour. The rudder is hinged at the leading edge, while the control lines are one foot from the rudder surface. (See Fig. 6.) Find: (a) the frictional resistance of the rudder when neutral, (b) the frictional resistance of the rudder when raised, (c) the frictional resistance of the rudder when set at an angle of 10° and its resistance at that angle, (d) the tension on the control lead under the same conditions as (b).

(a) The area of the rudder is $3\frac{1}{2} \times 4\frac{1}{2} = 15$ square feet. From Fig. 12 in Section 3, we see that the frictional resistance on a surface of 15 square feet at 60 miles an hour equals 6285 pounds per square foot. Thus the total frictional resistance is $15 \times 6285 = 401$ pounds.

(b) The aspect ratio of 150 (rudder 1.5). The distance from the leading edge to the center of pressure is given by Fig. 5. Interpolating between $L/D = 1$ and $L/D = 1.5$, we see that the center of pressure on a plate of aspect ratio 1.5 at an angle of incidence of 10° is 36% of the chord from the leading edge. Thus the desired distance is $21\frac{1}{2} \times .36 = 7.74$ feet. The moment arm about the center of gravity is $16 - 7.74 = 8.26$ feet. The total area about the center of gravity is $15 \times 1.5 = 22.5$ square feet. The total area about the center of gravity is $15 \times 1.5 = 22.5$ square feet. The total area about the center of gravity is $15 \times 1.5 = 22.5$ square feet.

By Figs. 1 and 4, $K_p = 0.0104$ and $L/D = 5.5$. Then L , the force perpendicular to the line of flight, is $K_p \cdot V^2 = 0.0104 \cdot 15 \times 3600 = 69.6$ pounds, and A , the moment, is $L \times D = 69.6 \times 8.26 = 576$ foot-pounds. It will be seen that turning the rudder a decided increase in the resistance of the surface.

The above work gives us a basis for rapidly computing the turning moment. $M = 26.8 \times 18.8 \times 14 = 727$ foot-pounds, taking the maximum of both the lift and the drag, then the center of gravity.

(c) The turning moment about the leading edge of the rudder is $0.89 \times 60 \times 36 \times 0.116 = 80$ at 30° = 33 foot-pounds.

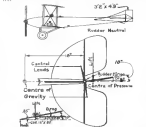


FIG. 8. RUDDER AND ELEVATOR IN FLAT PLANE. INCREASE IN RESISTANCE AND MOMENT OF LEADING EDGE

Minimum area of control lead on one 18" = 584 feet. Then, since the stress in the control lead from the center area must just balance the turning moment of the rudder set at an angle, tension in lead = $\frac{576}{18} = 32$ pounds.

General Considerations of Sustaining Power and Resistance of Wing Section

We have seen that the equation for lift is $L = K_p \cdot V^2$ (1)

where K_p is a constant varying with the angle of incidence, V is airspeed in feet per second, and L is lift in pounds. The lift is equal to the weight of the aircraft, W , and the equation becomes

$$W = K_p \cdot V^2 \quad (2)$$

which can be expressed in the form

$$K_p = \frac{W}{V^2} \quad (3)$$

$$L = \frac{W}{V^2} \cdot V^2 \quad (4)$$

$$L = W \quad (5)$$

as may be perceived. The lift coefficient is equal to the aspect ratio and increases at larger angles until the "break" point is reached.

a critical angle is reached, so can be seen from the curve of a typical wing section (B & F 4) in Fig. 9.

From these considerations may be deduced the following data, which should become absolutely familiar to every student of aerodynamics.

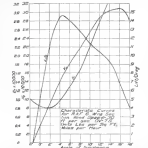


FIG. 9. CHARACTERISTIC CURVES FOR B & F 4 WING SECTION

A surface traveling fast will require by equation (3), a small value of K_p , and hence a small angle of incidence. Conversely, flying slowly it will require a large angle of incidence. In other words, a given weight, at a given angle of incidence and other area or speed.

If we give a machine a large wing area, it will fly slowly with a small angle, and it will attain a high velocity if sufficiently small power is available.

The drag equation is

$$D = K_d \cdot V^2 \quad (6)$$

The higher the value of L/D , the smaller will be the drag for a given lift and weight of machine at a given speed, and the less will be the power required. The ratio L/D is therefore a measure of the efficiency of the wing. For the B & F 4, the maximum value of L/D is at about 4° and at about this angle a surface would fly at its greatest efficiency.

We have here understood all other resistance to that of the wing. These resistance will modify the drag coefficient and the best angle of flight. We shall deal with these modifications under the Resistance Losses of Flight.

Problem of Sustaining and Resistance of Wing Surface

A monoplane weighing 2000 pounds runs on B & F 4 wing section.

(a) What area will it require so that its lowest speed may be 40 miles an hour?

(b) What will be the drag of the wing at this speed and what will be the horsepower required for the wing alone?

(c) Assuming that the parasite resistance (resistance of the landing chassis, wires, etc., etc.) is 120 pounds at 60 miles an hour, and that it varies directly as the square of the speed, what will be the total resistance and horsepower required at this speed?

(d) If the power delivered at the propeller is 100 horsepower, what is the maximum speed available?

(e) Let A = wing area

B = wing of machine

D = drag of wing

P = parasite resistance

R = total resistance = $D + P$

From Fig. 9 we see that the maximum value of K_p is 0.0606, at 10°. Then, since $W = K_p \cdot V^2$, and $V = 45$ miles per hour, $4 = \frac{W}{K_p \cdot V^2} = \frac{2000}{(0.0606 \times 45^2)} = 319$ square feet.

(b) From Fig. 9, L/D at 10° = 5.8. Then $L = \frac{2000}{5.8} = 345$ pounds.

Since $\frac{1}{115}$ horse-power is required to overcome a resistance of 1 pound of 1 mile per hour, horse-power = $\frac{345}{115} = 3$ horse-power to overcome wing drag of 345 miles per hour.

The drag of the wings can also be obtained, of course, by substituting the proper value of K_d in the equation

The first method described will show the simpler when a number of cases are to be worked out, but the second is more accurate at very small angles of incidence.

(c) At 60 miles an hour $K_p = \frac{W}{V^2} = \frac{2000}{(60^2)} = 0.0556$.

Fig. 9 shows that the value of K_p will be attained at an angle of incidence of 5.7°, at which angle $L/D = 14.2$.

Then $D = \frac{W}{L/D} = \frac{2000}{14.2} = 141$ pounds, and $R = D + P = 141 + 120 = 261$ pounds.

The power required equals $\frac{R}{115} = \frac{261}{115} = 2.27$ horse-power.

In order to determine accurately the speed obtainable with a given power, it is necessary to plot a curve of power required at various speeds. In computing points on this curve, we assume the parasite resistance proportional to V^2 . This is approximately true, the deviation being due to changes in resistance coefficients of both, ailerons, etc., as the angle at which they meet the wind changes. Proceeding on this assumption, $K = K_p \cdot V^2$, since $P = 120$ pounds when $V = 60$ miles per hour, $K = \frac{P}{V^2} = \frac{120}{60^2}$, and $P = 400K$.

In Table 2 are given a few points on such a curve, computed as was that for 60 miles an hour, which we just solved. A student might carry through some of these computations, checking the results against those here given, in order to make sure that the method is perfectly sound in this.

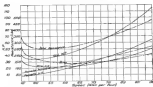


FIG. 10. REQUIREMENT, HORN-POWER AND SPEED DIAGRAM

TABLE 2

V	A ₀	W	K _p	L/D	P	R	W/R	W/P	W/R	W/P
45	0.0606	2000	0.0606	5.8	141	261	7.68	5.0	42.5	5.0
60	0.0556	2000	0.0556	14.2	141	261	7.68	5.0	42.5	5.0
75	0.0500	2000	0.0500	14.2	141	261	7.68	5.0	42.5	5.0
90	0.0455	2000	0.0455	14.2	141	261	7.68	5.0	42.5	5.0
105	0.0417	2000	0.0417	14.2	141	261	7.68	5.0	42.5	5.0
120	0.0385	2000	0.0385	14.2	141	261	7.68	5.0	42.5	5.0
135	0.0357	2000	0.0357	14.2	141	261	7.68	5.0	42.5	5.0
150	0.0333	2000	0.0333	14.2	141	261	7.68	5.0	42.5	5.0
165	0.0311	2000	0.0311	14.2	141	261	7.68	5.0	42.5	5.0
180	0.0293	2000	0.0293	14.2	141	261	7.68	5.0	42.5	5.0
195	0.0277	2000	0.0277	14.2	141	261	7.68	5.0	42.5	5.0
210	0.0263	2000	0.0263	14.2	141	261	7.68	5.0	42.5	5.0
225	0.0250	2000	0.0250	14.2	141	261	7.68	5.0	42.5	5.0
240	0.0238	2000	0.0238	14.2	141	261	7.68	5.0	42.5	5.0
255	0.0227	2000	0.0227	14.2	141	261	7.68	5.0	42.5	5.0
270	0.0217	2000	0.0217	14.2	141	261	7.68	5.0	42.5	5.0
285	0.0208	2000	0.0208	14.2	141	261	7.68	5.0	42.5	5.0
300	0.0200	2000	0.0200	14.2	141	261	7.68	5.0	42.5	5.0

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WILLIAM FOSTER BROWN, sailmaker and amateur aviator, recently passed by his instructor, FRANCIS BROWN, from a second class to a first class flying boat. Brown, a resident of New York, had been flying for two years and had just completed his first solo flight. Brown, after he started his own business, was out of sight of the flying boat on the water when he was seen. He made an average speed of forty miles an hour and landed under ideal conditions with the motor working smoothly along the entire journey of 100 miles. Mr. Brown and his instructor made a perfect landing on the flying boat of the American Transportation Company at Manhattan Bay. He intends to devote considerably more time to aviation and has just placed an order for his new Curtiss tractor.

Captain RALPH McMELEN, head of the Aviation Corps of the United States Army, was killed in a flight in his Curtiss biplane on September 2. R. E. McMELEN plans to establish an aviation school and airplane factory at Great Falls, Mont.

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